
Efficient Feed for Offset Parabolic Antennas for 2.4 GHz

Dragoslav Dobričić, YU1AW

Resume

This article examines some of the possible solutions to the problems of efficiently illuminating SAT TV offset parabolic antennas in the use on WLAN frequencies of 2.4 GHz..

Introduction

The problems that occur while illuminating shallow offset parabolic dishes, in addition to those related to the efficient use of parabolic dishes generally are additionally aggravated by the specific geometry of the parabolic mirror itself. [2] Feed positioning in the way that its phase center exactly coincides with the focus of the offset parabolic dish and its aiming so that the radiation maximum falls in the geometric center of the elliptic reflector surface are not intuitive at all, as in classic parabolic antennas. Therefore, there is much confusion and many wrongly positioned feeds that do not correctly illuminate offset parabolic dishes, decreasing their efficiency and gain.

The optimal feed for some given parabola has to fulfill several important characteristics:

1. The radiation angle of the main beam, between the points in which the gain is -10dB in relation to the maximal value, has to match the subtended angle. The feed radiation angle, both in horizontal and in vertical plane has to be the same, regardless the ellipticity of offset parabola.
2. The phase center of the feed has to be well defined and stable with changes of frequencies within the working range. The change of the phase within the whole angle of illumination has to be as small as possible.
3. The feed characteristics must not change much in the presence of the parabolic reflector and carrier structure.
4. Feed radiation diagram has to be very clean, i.e., with low side lobes and rear lobes.
5. The feed structure has to encroach as little as possible into the focal cone, i.e. in the space between focus and the antenna surface. Therefore, it is good when the feed phase center is on the front edge or directly in front of the antenna structure.

It is not easy at all to accomplish all these demands. The efficiency and gain of parabolic antennas directly depend on the mode of accomplishing these demands. Therefore, in practice, it is common to make good feed first and then to choose or make a parabolic reflector with a F/D value that fits the best with the feed. [4, 5] However, if you want to use the cheap production of SAT TV offset parabolas for the work on HAM or WLAN frequencies; you have to try to construct a feed that matches those parabolic reflectors. SAT TV antennas usually have F/D in band from 0.7 to 0.9.

For efficient illumination, we need a feed with a clean diagram that has equal width of the main beam in both planes and gain of about 12-14 dBi. This fact at the start excludes some antennas as efficient feeds for SAT TV offset parabolas. Among them is, for example, the coffee can (simple open circular waveguide) antenna that has gain of about 6-7 dBi and is very inefficient as

a feed for offset parabolas. It is acceptable only for parabolas that have F/D less than about 0.5. The bi-quad antenna is somewhat better, with its gain of about 10 dBi, and its optimal version with evened diagrams in both planes and a gain of 11 dBi is even better.

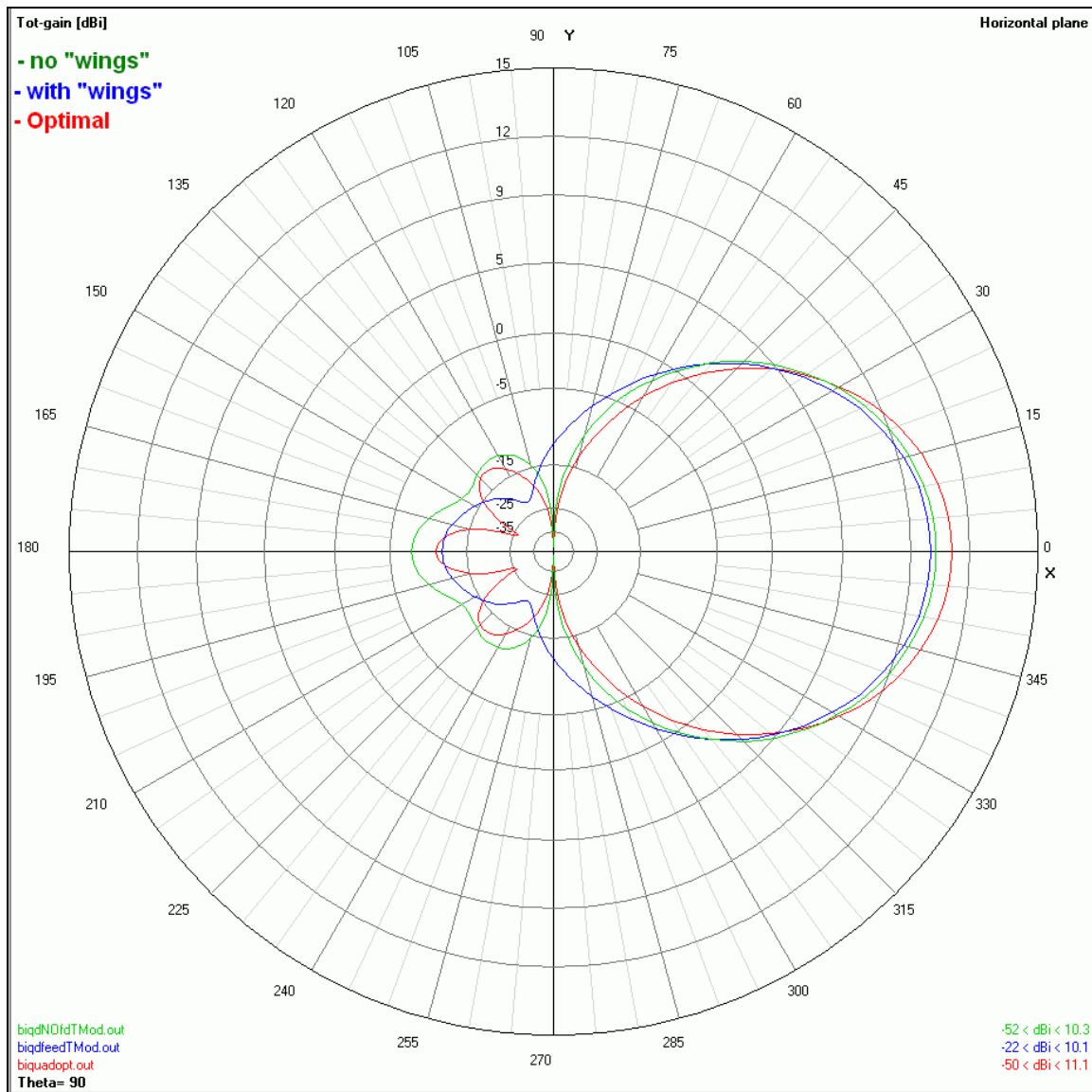


Fig. 1. Horizontal diagram of bi-quad antenna with and without “wings“ and optimal bi-quad with evened diagrams.

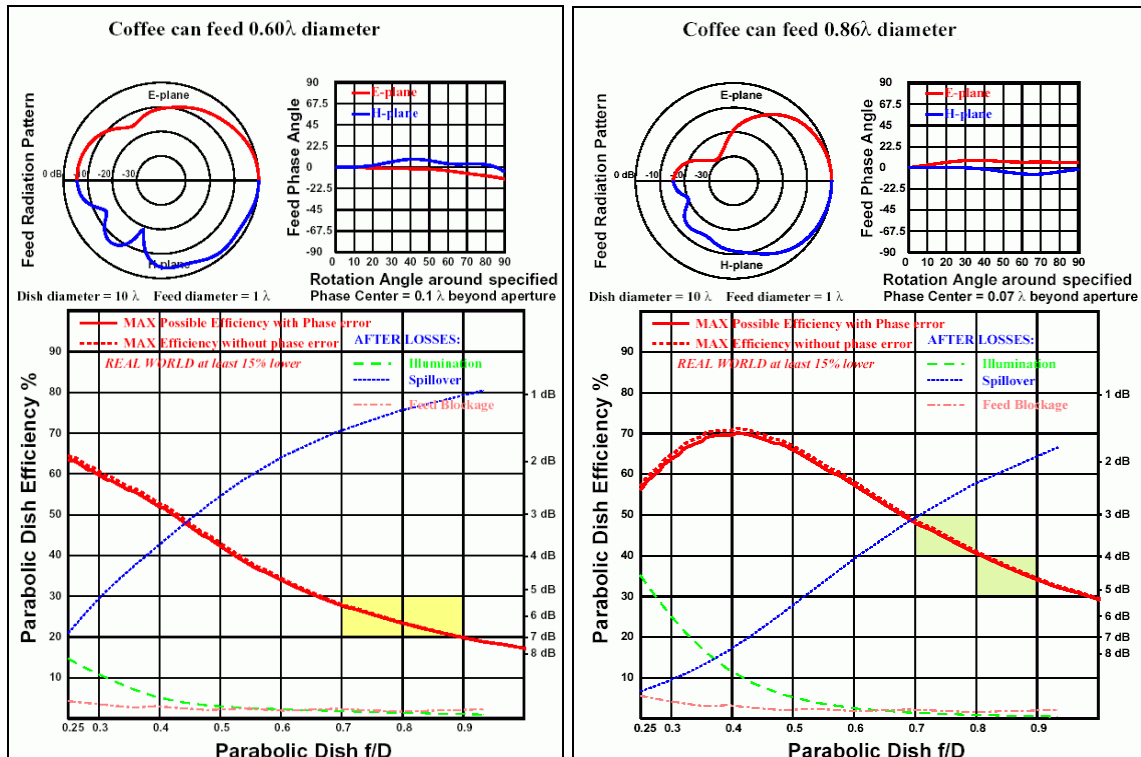


Fig. 2. Efficiency of coffee can antenna feed with different waveguide diameter

I presented some diagrams of efficiency of some antennas that are used as feeds for parabolas with different F/D and it is very clear how efficiently they work with offset dishes whose F/D is in the band 0.7-0.9 (colored band). For example, it is clear that an offset parabola with a coffee can antenna whose diameter is 0.6 wavelengths, i.e. about 74 mm at 2.45 GHz, has an efficiency of about 25%, a value that consequently decreases the gain of antenna by 6 dB in relation to its theoretic value. That is exactly how much it would be gained with twice as small, efficiently illuminated offset parabola! [3] Even coffee can antennas with a diameter of 0.86 wavelengths, or 106 mm, do not work brilliantly. They give about 4 dB loss of antenna gain in relation to the theoretic value with an efficiency of 100%. Greater diameters of coffee can antenna have problems with the appearance of higher modes of EM waves and consequently very problematic diagrams and phase centers, so they have not recommended. The addition of conic funnel can partially improve the situation, but such **horn** antennas have uneven diagrams in the vertical and horizontal planes, which is very undesirable for antennas that pretend to be good and efficient feeds for dish.

The **bi-quad antenna** is somewhat better feed for offset parabola than coffee can antenna. Adding “wings” to reflector, which some authors use in order to improve illumination efficiency of dish, change only back side lobe radiation. The front diagram is almost unchanged and as a feed it has unchanged efficiency. The **optimal bi-quad**, according to **L.B. Cebik** [1], with reflector dimensions 150x200 mm, is even better and gives about 5% higher efficiency than other variants of bi-quad.

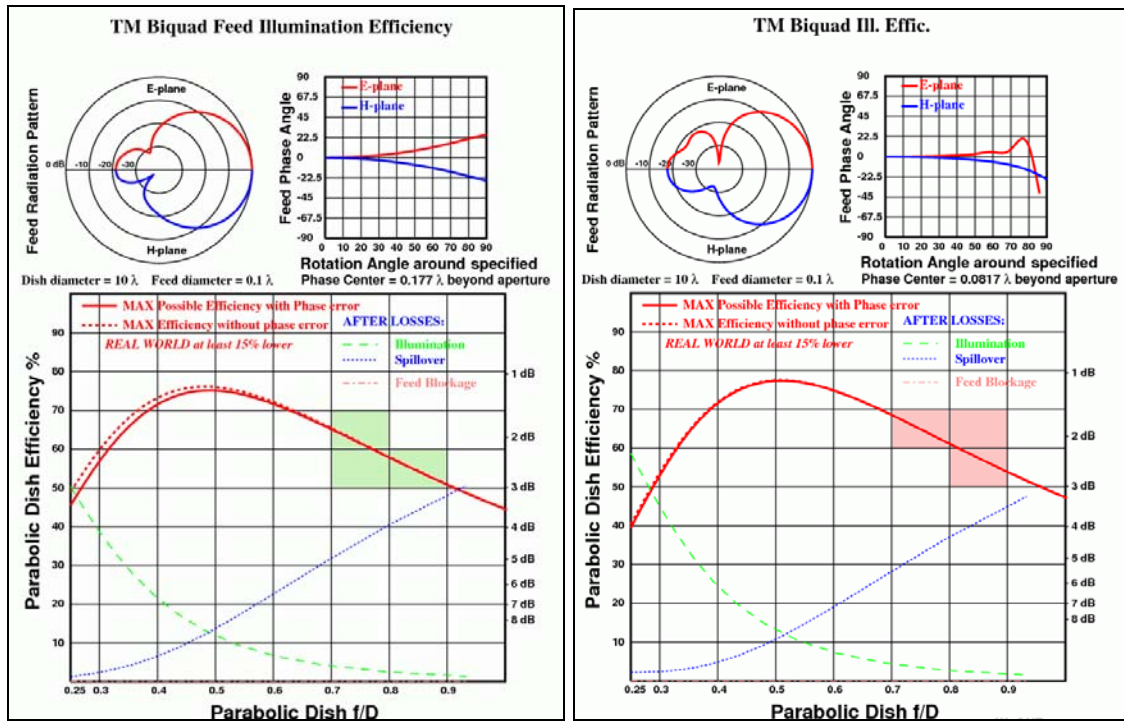


Fig. 3. Bi-quad antenna feed efficiency with “wings” (left) and without “wings” (right)

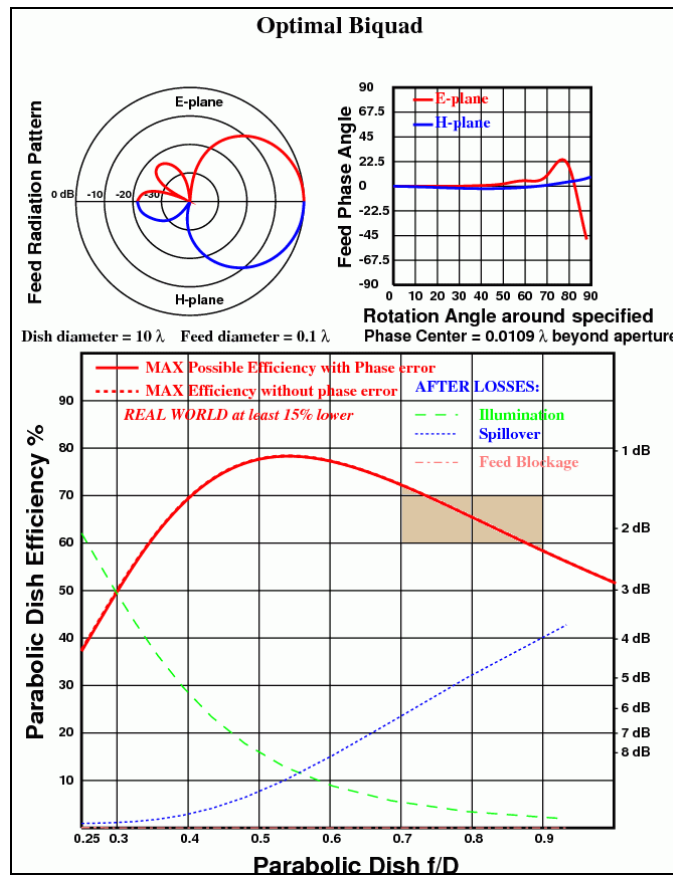


Fig. 4. Efficiency of optimal bi-quad as feed for offset dish

Two-element bi-quad feed for 2.4 GHz

As shown in the picture above, the optimal bi-quad has very high efficiency when it is illuminating dishes whose F/D is 0.5-0.6. It is obvious that it could also be adjusted for dishes with higher F/D, if the diagram could be narrowed in both planes and at the same time retain all other good characteristics. Since narrowing of the diagram, i.e. increasing of gain of the antenna, is possible only by addition of director element, that was the course I took. However, the addition of a resonant parasitic element as a director to this relatively complex structure was not such an easy thing to do! I found and looked at several reported two-element bi-quads on the Internet and by short analysis I realized that neither of them had nearly optimal performances. Some of them even worked worse with an added director than without it!

By detailed analysis and optimization I realized that director has to have approximately the **same electrical length as the active element** if you want to retain an optimal diagram for use with an offset parabola. With different dimensions of the director and distances between elements, somewhat higher gain can be achieved, but then the diagram is not optimal for the illumination of the offset parabolas. Also, the reflector has to be increased in relation to the one in the optimal bi-quad and is square shaped with the side of 1.6 wavelengths. Some minor asymmetry in horizontal plane diagram of two-element bi-quad feed antenna is due to asymmetrical feeding of antenna radiator.

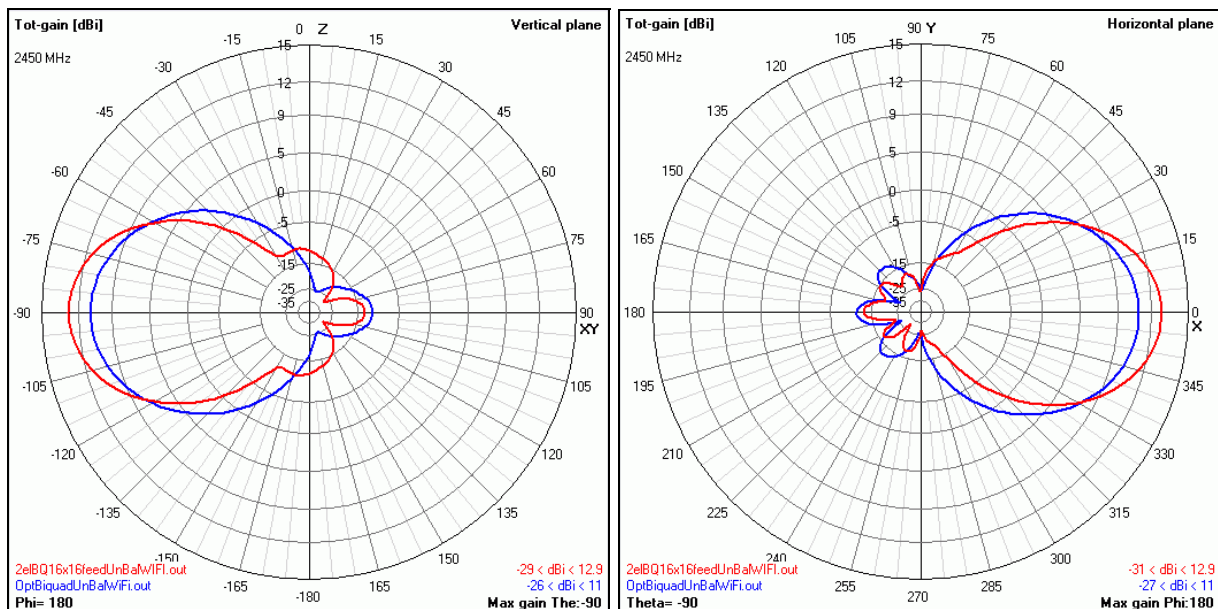


Fig. 5. Horizontal and vertical diagrams of optimal bi-quad and 2 element bi-quad feed

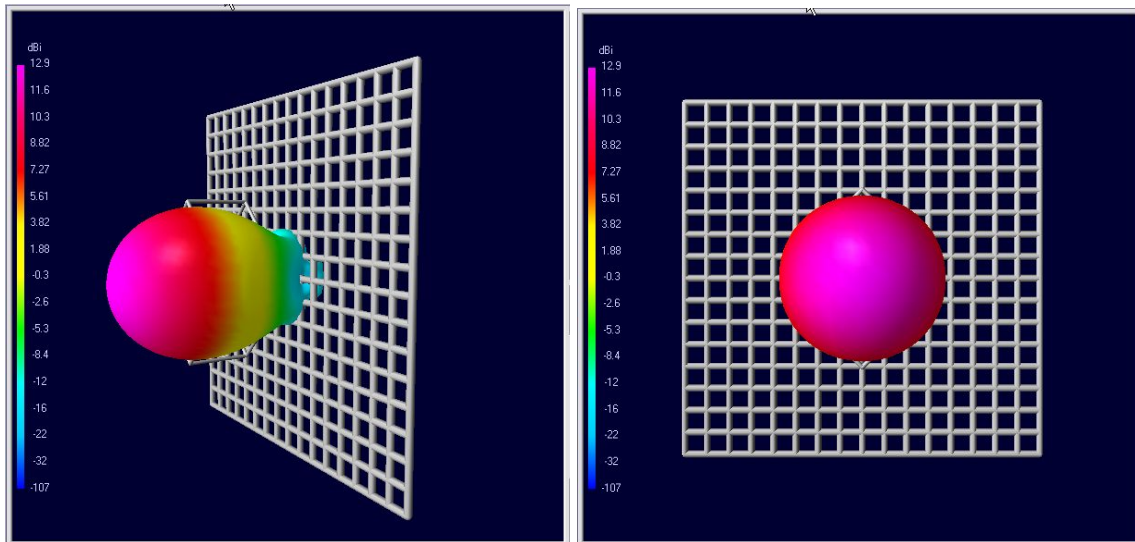


Fig. 6. Side and front view of 2-element bi-quad feed diagrams

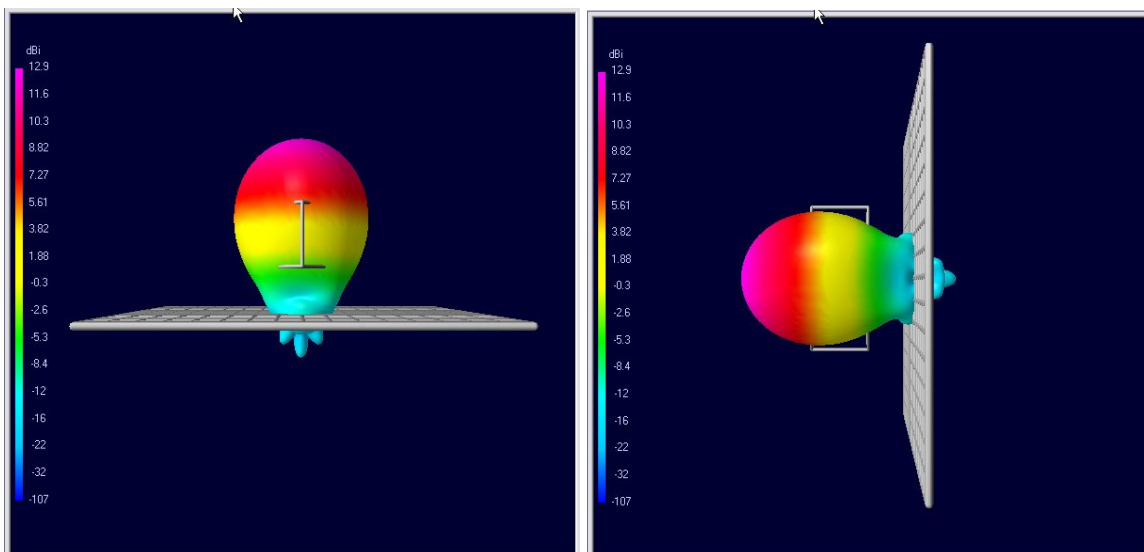


Fig. 7. Horizontal and vertical diagram of 2-element bi-quad feed

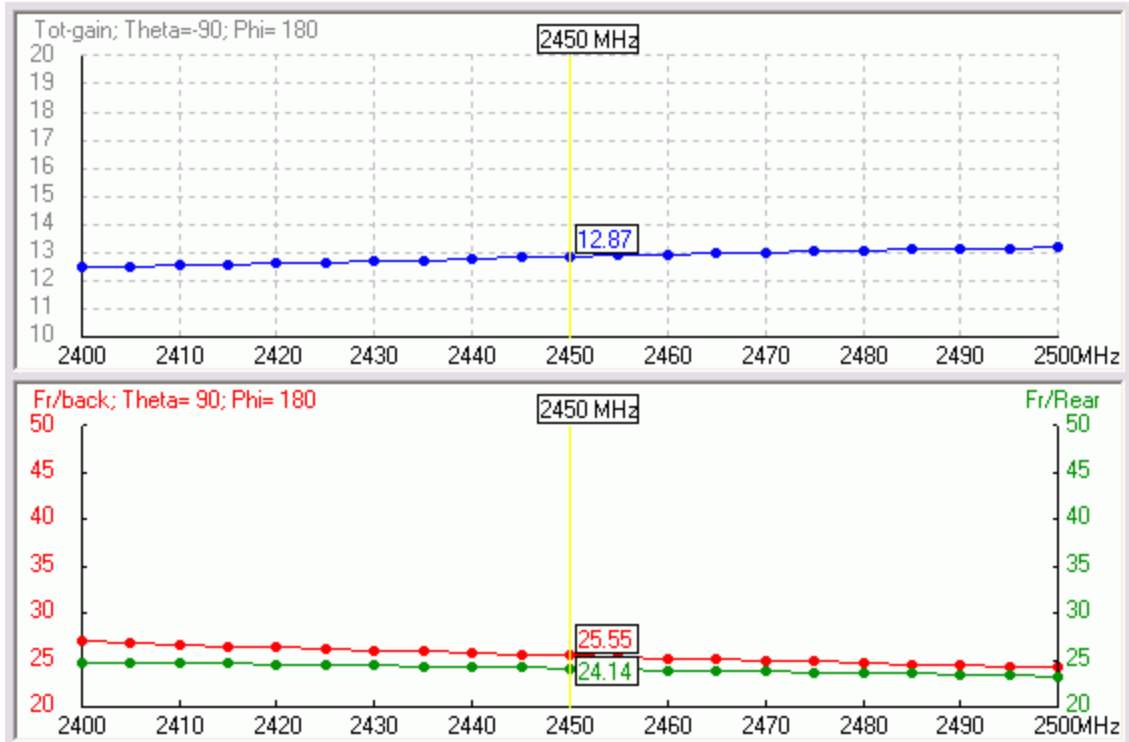


Fig. 8. Gain, F/B and F/R of 2 el. bi-quad feed for different frequencies

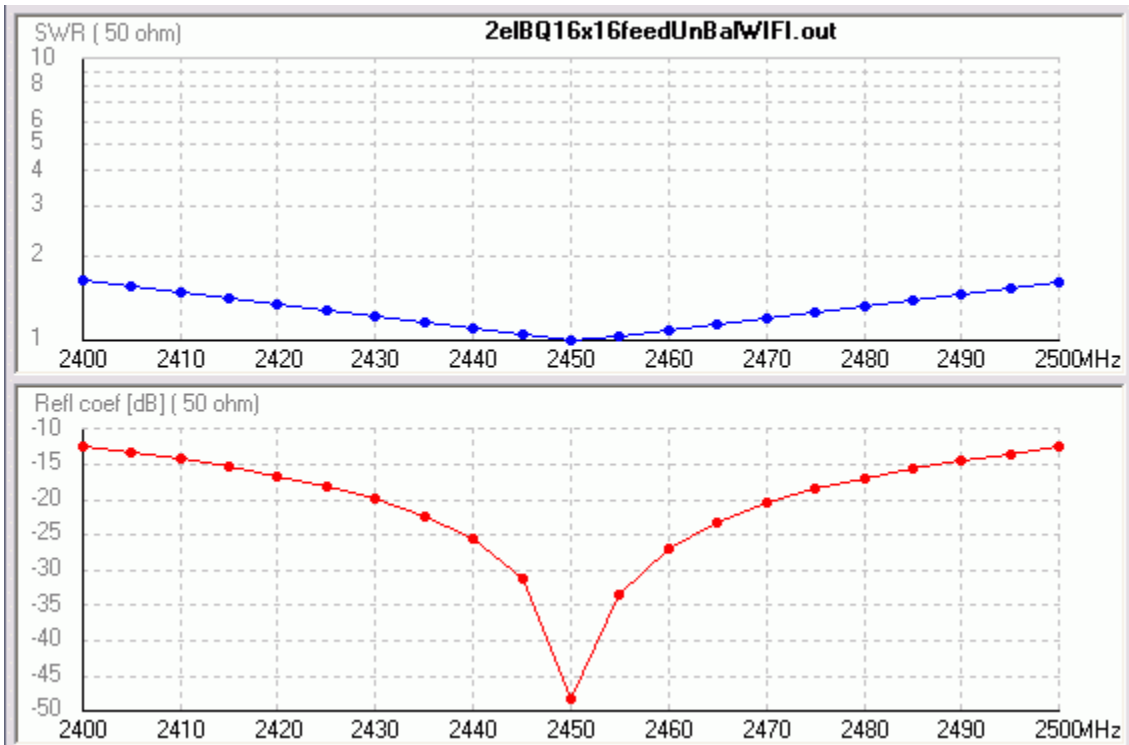


Fig. 9. SWR and Reflection coefficient of 2 el. bi-quad feed for different frequencies

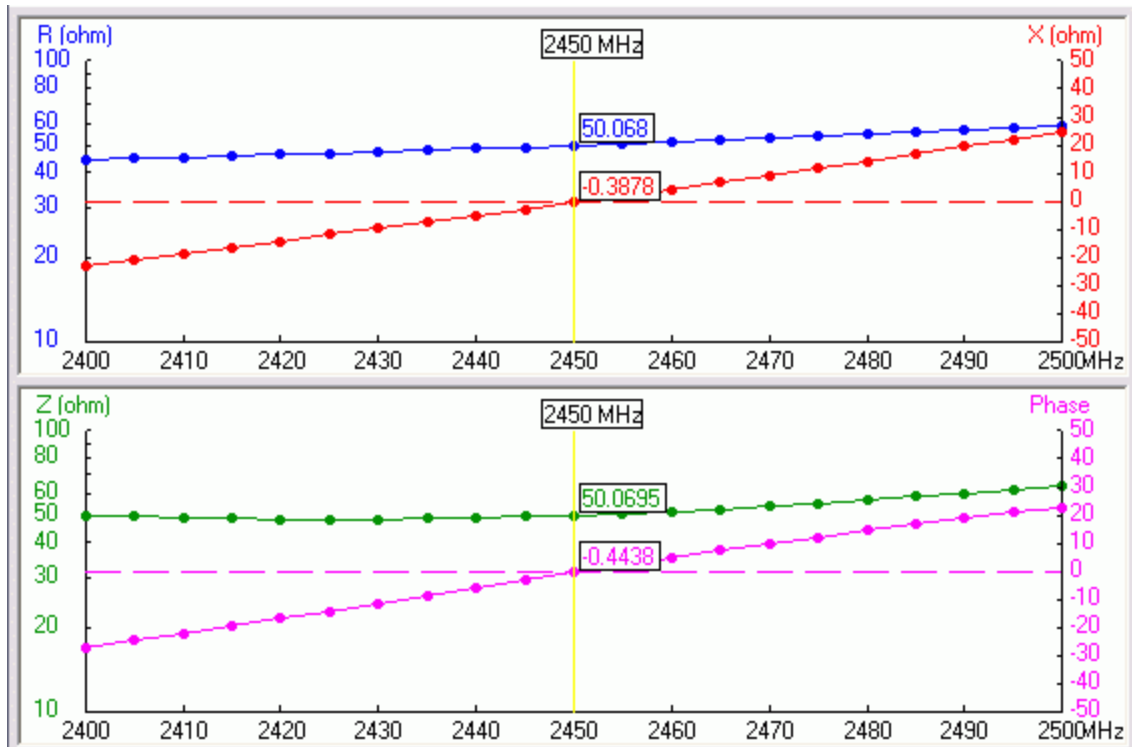


Fig. 10. Input impedance of 2 el. bi-quad feed for different frequencies

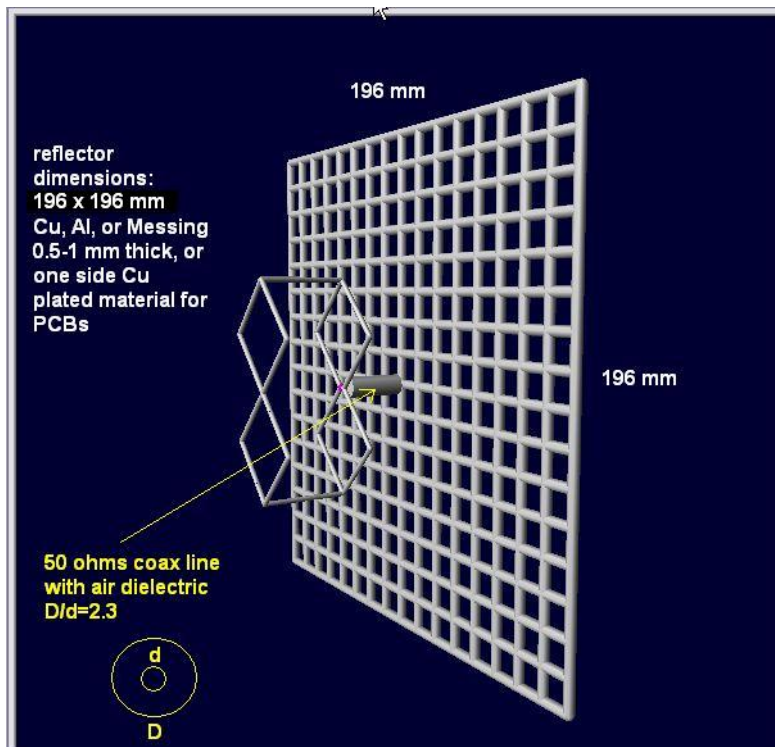


Рис. 11. Внешний вид двухэлементного биквадрата с размерами рефлектора

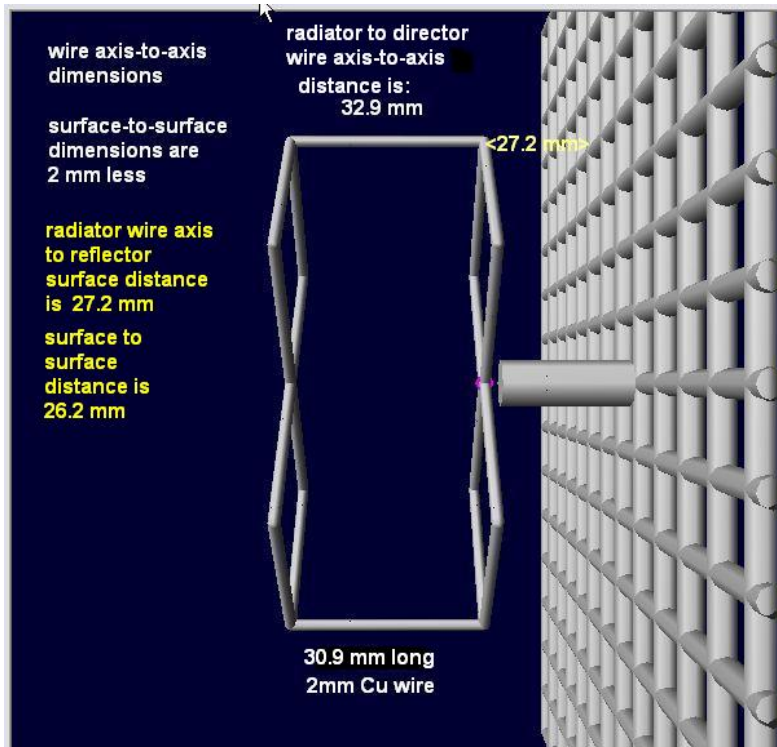


Рис. 12. Расстояния между элементами

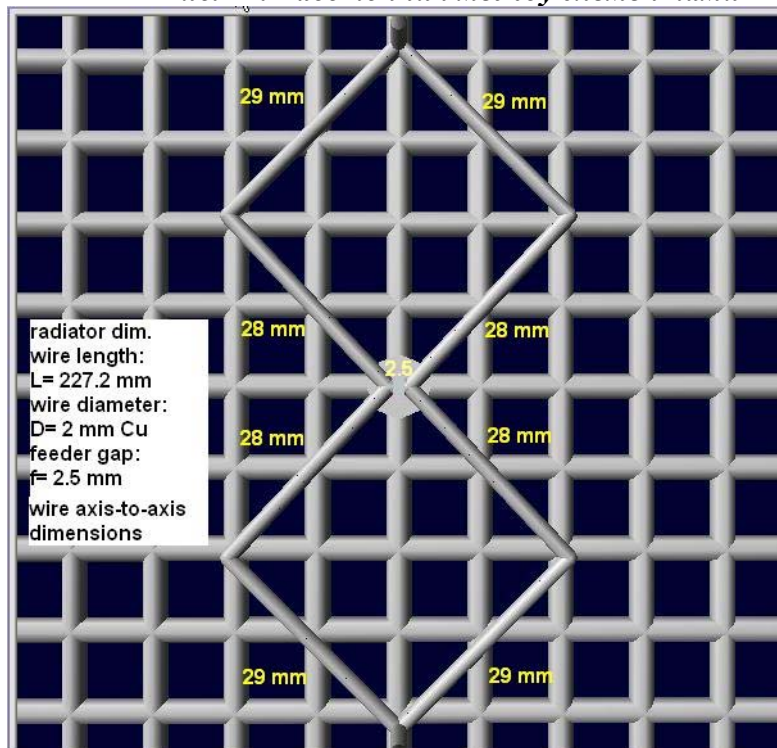


Рис. 13. Размеры вибратора

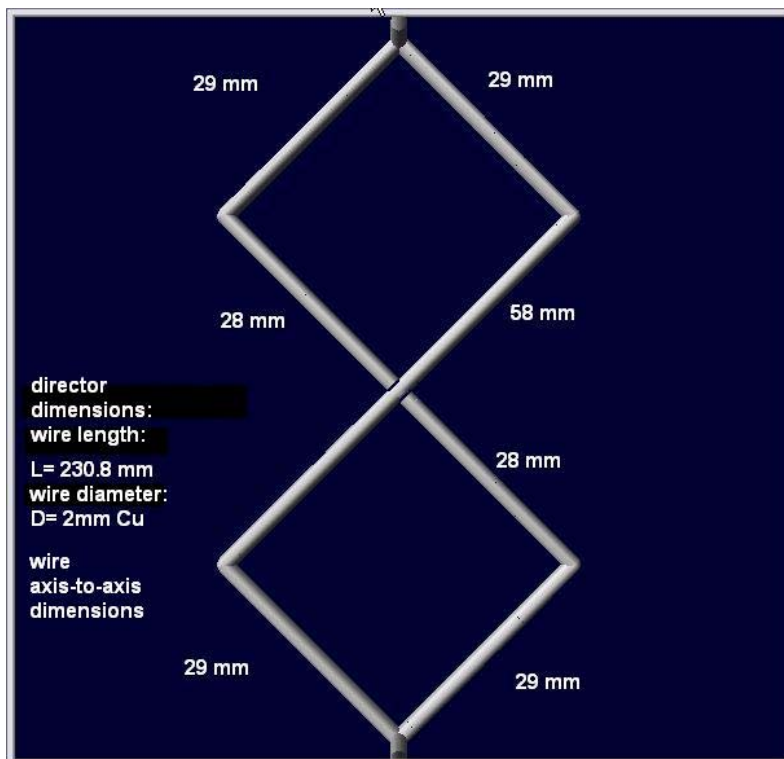


Рис. 14. Размеры директора

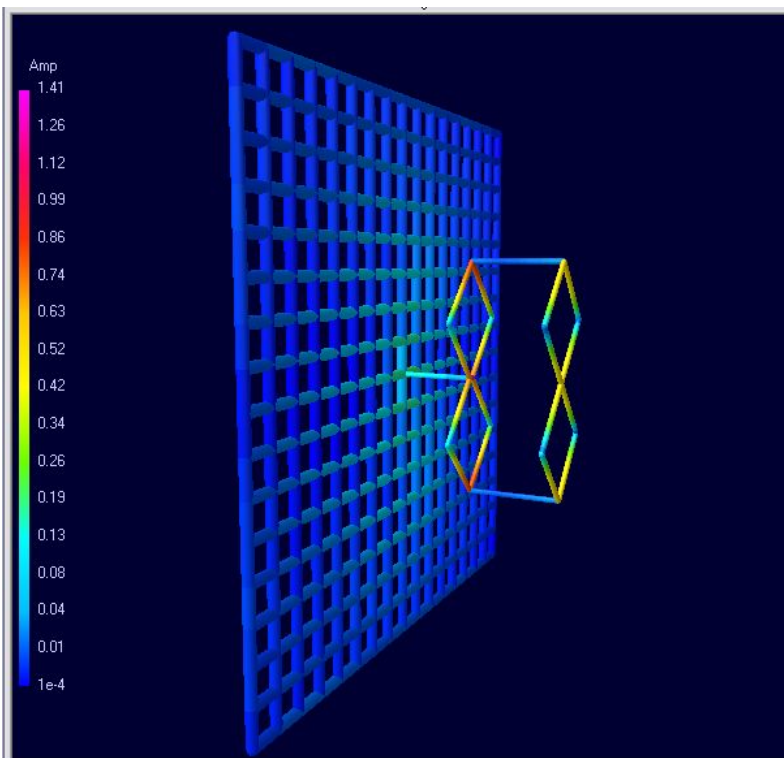


Рис. 15. Токи в двухэлементном биквадрате при подведённой мощности 100 W

Механическая конструкция антенны.

Вибратор и директор изготавливаются из двух кусков медного провода, диаметром 2-2.3 mm и общей длиной 227.2 mm для вибратора и 230.8 mm для директора. Оба куска провода сгибаются как показано на иллюстрациях.

Вибратор сгибается в форме биквадрата т.е. концы провода соединяются в центре вибратора под углом 90 градусов .

Директор согнут в форме цифры 8 и концы провода "встечаются" в центре "восьмёрки" с противоположных сторон.

Перед сгибанием нужно отмерить и отрезать необходимые куски медного провода с максимальной возможной точностью и затем измерить и пометить точки в которых будет производиться сгибание.

Концы провода директора спаиваются вместе в местах соприкосновения.

Рефлектор может быть изготовлен из листовой меди или латуни. Можно использовать одно-сторонний фольгированный стеклотекстолит . Две перемычки соединяющих между собой вибратор и директор имеют длину 30.9 mm, при условии что провод для изготовления элементов антенны имеет диаметр 2 mm. Они припаиваются непосредственно к элементам как показано на рисунке.

Такое решение делает сборку несложной но в тоже время обеспечивает достаточную механическую прочность антенны.

Важно помнить что размеры приведённые на рисунках даны от оси до оси проводов.

Размеры от поверхности до поверхности проводов уменьшены на 2 mm!

Расстояние между вибратором и рефлектором дано от оси провода вибратора до поверхности рефлектора.

От поверхности провода вибратора до поверхности рефлектора расстояние меньше на 1 mm, т.е. 26.2 mm! Также точно размеры перемычек скрепляющих вибратор и директор даны с учётом расстояния между осями проводов этих элементов.

Чтобы выдержать межосевое расстояние перемычки должны быть короче его на 2 mm, т.е. 30.9 mm!

Питание.

Питание биквадрата может быть выполнено несколькими способами. вибратор может быть установлен на коаксиальную линию из медного провода и медной или латунной трубки, с соотношениями их диаметров приблизительно 1:2.3 при этом её волновое сопротивление составит 50 ом медный провод диаметром 2.3 mm и медная трубка с внутренним диаметром 5 mm имеют оптимальное сочетание диаметров.

В рефлекторе сверлится отверстие диаметром 5,5 мм и трубка паяется к рефлектору в круговую с фронтальной стороны рефлектора. Провод должен быть припаян к центральному соединителю коннектора с одной стороны и к вибратору с другой. При этом по отношению к стенкам трубки провод должен располагаться с максимальной коаксиальностью.

Also, instead of complete air coax, one can solder only the tube through which coax cable without its outer plastic jacket comes in tightly, so that outer conductor rests tightly to the inner wall of the tube. After that, the braid is soldered well to the both sides of the tube. If you use cable with larger diameter that is stiff enough, or semi-rigid cable, only the end of the cable without its outer plastic jacket can be pulled through reflector and soldered to the reflector surface at the place where the cable passes through the reflector.

“ “ “ 0

Чтобы медь не темнела и не было коррозионных явлений лучше всего покрыть антенну тонким слоем прозрачного лака. Перед этим, точки где припаян кабель и места пайки в перекрестьях элементов нужно защитить тонким слоем полиэтилена, используя для этого специальный термопистолет.

Слой полиэтилена обеспечит защиту от воды, но он должен быть максимально возможно тонким! Неоправданное увеличение слоя полиэтилена особенно на местах соединений только увеличит рассогласование антенны! Также, строго запрещено применение силикона, так как он химически агрессивен и вносит большие потери на высоких частотах!

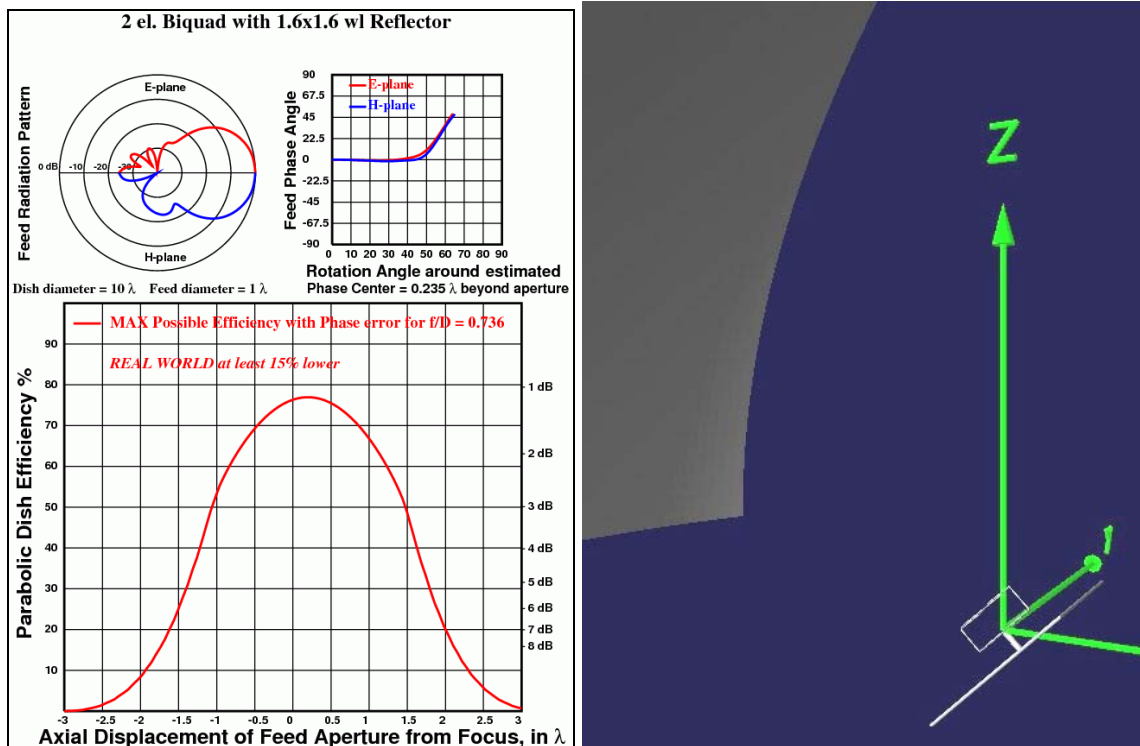


Fig. 16. Two-element bi-quad feed phase center allocation and its position at dish focus point

“ “ “ 0

В стандартном биквадрате, фазовый центр находится у плоскости рефлектора. В случае же двухэлементного биквадрата, так как добавлен директор, фазовый центр смещён к вибратору. При исследовании позиции фазового центра двухэлементного биквадрата выясняется что он располагается на расстоянии 0.235 длины волны или 29 mm впереди рефлектора. Это приблизительно соответствует точке питания вибратора. Данная точка должна быть помещена в фокус параболы с максимально возможной точностью. Направление максимального излучения основного лепестка должно быть направлено в геометрический центр эллиптической поверхности офсетной параболы.

When SAT TV offset parabolas are used, focus is determined by the position of the SAT TV converter. Focus of the parabola, practically, is in the entrance in the waveguide of the converter. By measuring the distances between the entrance of the converter and at least 3 fixed points at the edges of the parabola, one should keep the information about the position of the focus, so that it could be precisely determined and restored when the SAT TV converter and original carrier are taken off or adjusted in order to be able to carry a different feed. This is very important because it is very often that case that, after the correction of the feed carrier, the position of the parabola's focus is lost and it can not be restored if there is no information, i.e. space coordinates in relation to parabolic surface.

Results with offset parabola

We achieved very good results by analysis of two-element bi-quad as feed of rectangle shaped offset parabola, with dimensions 100x120 cm and $F/D=0.75$. We confirmed very high efficiency on the basis of achieved gain of parabolic antenna in relation to theoretic value. The calculation of the efficiency of illumination of parabola from its gain gave the value of about 77%, which well coincides with calculations of efficiency derived from the shape of the feed diagram given in Figure 18.

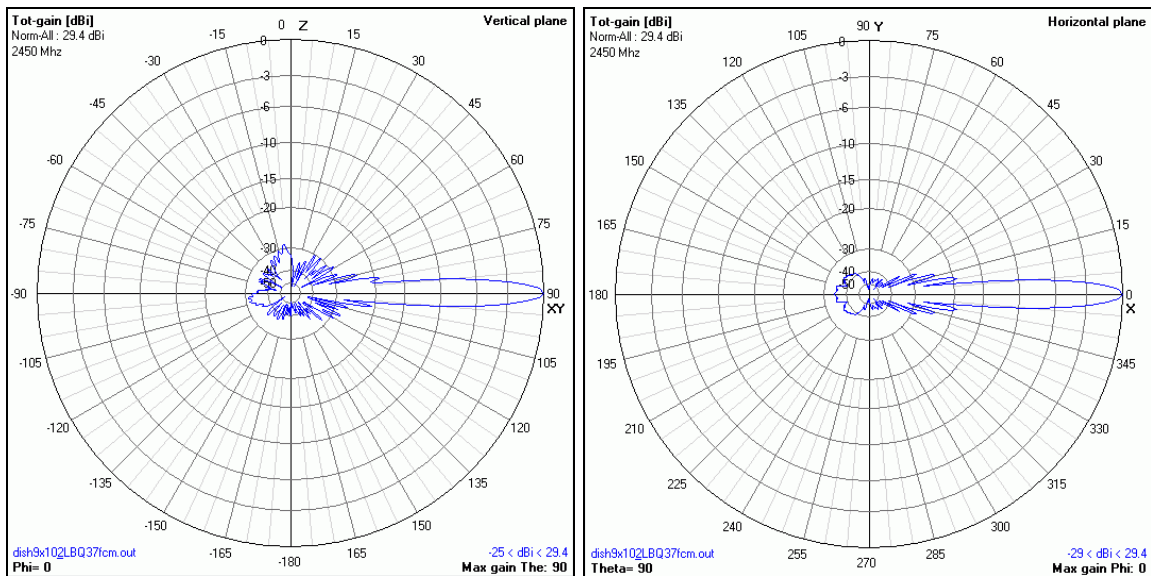


Fig. 17. Vertical and horizontal diagram of offset dish with 2 el. bi-quad feed

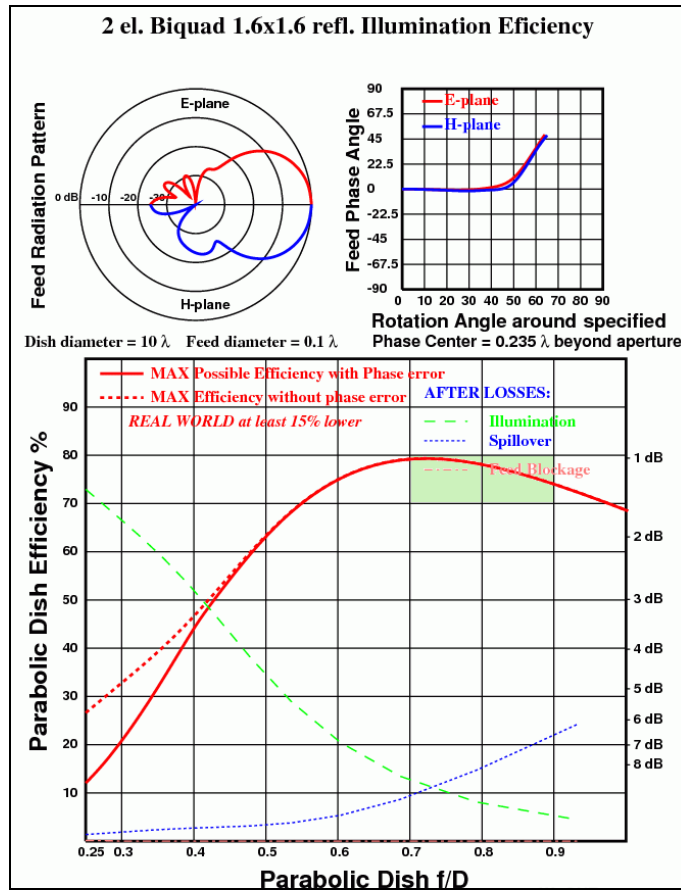


Fig. 18. Efficiency of 2 el. bi-quad feed with parabolas having different F/D ratio

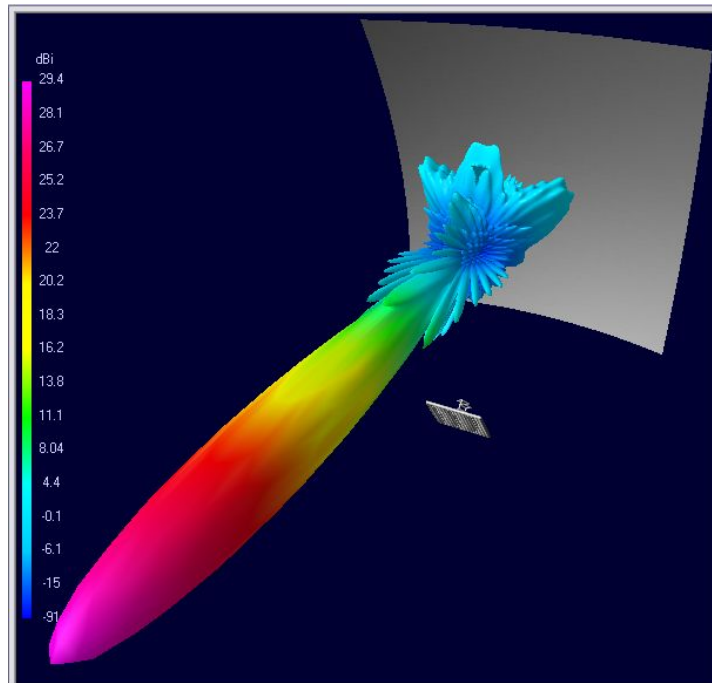


Fig. 19. 3D diagram of offset parabola with 2 el. bi-quad feed

An elliptic parabola with the same dimensions would have a smaller gain by about 1 dB in relation to this analyzed rectangular version, with the same efficiency, because of the somewhat smaller geometric surface of elliptic parabola. Another confirmation that this is a very good feed is the purity of achieved radiant diagram of parabola. First side lobes are suppressed by about 20 dB and the front to back ratio is about 30 dB.

Maximal gain of the antenna is achieved when the phase center of the feed is exactly in the focus of parabola and when the axis of bi-quad, i.e. maximum of radiant diagram of the main beam is aimed directly into the geometric center of parabolic surface that is in the crosshair of the large and small axes of the ellipse. The input impedance of bi-quad remained practically unchanged when placed in focus of parabola, which was expected from this antenna that is known by its relatively low Q factor.

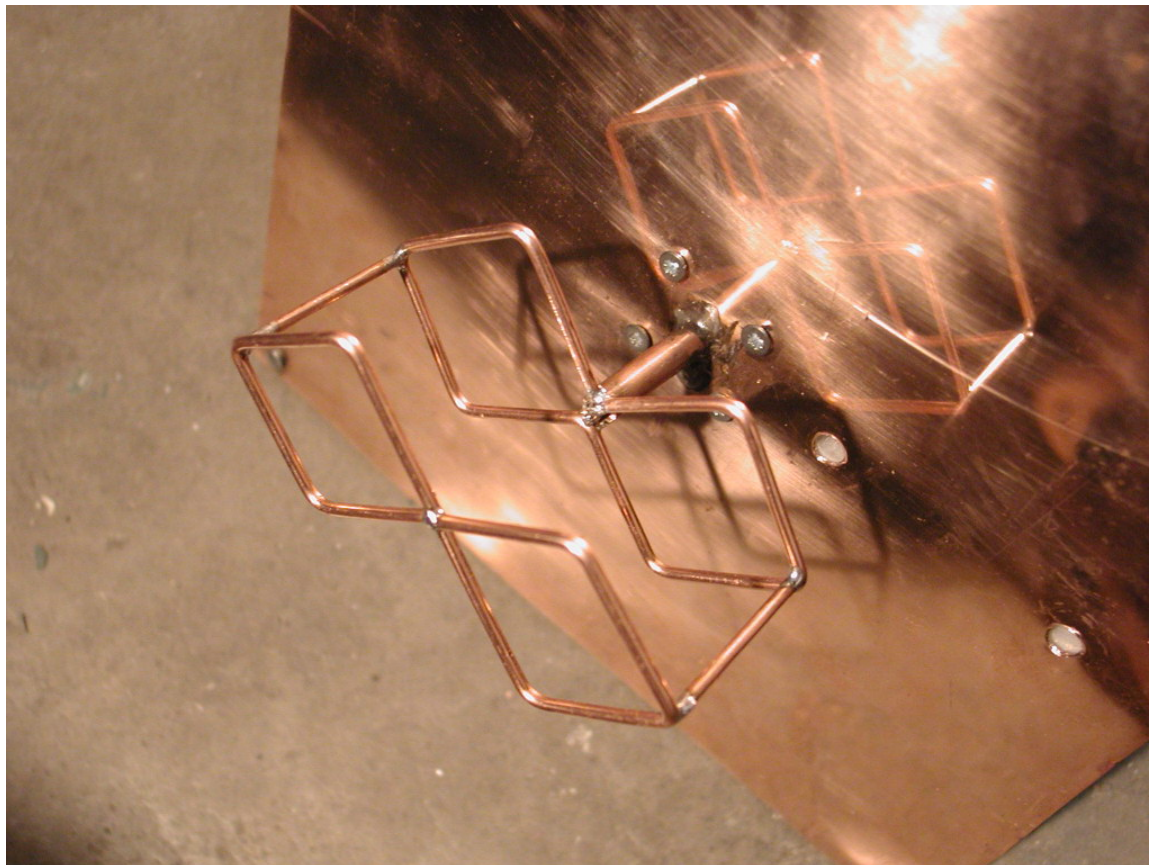


Fig. 20. Outlook of built 2 el. bi-quad feed antenna

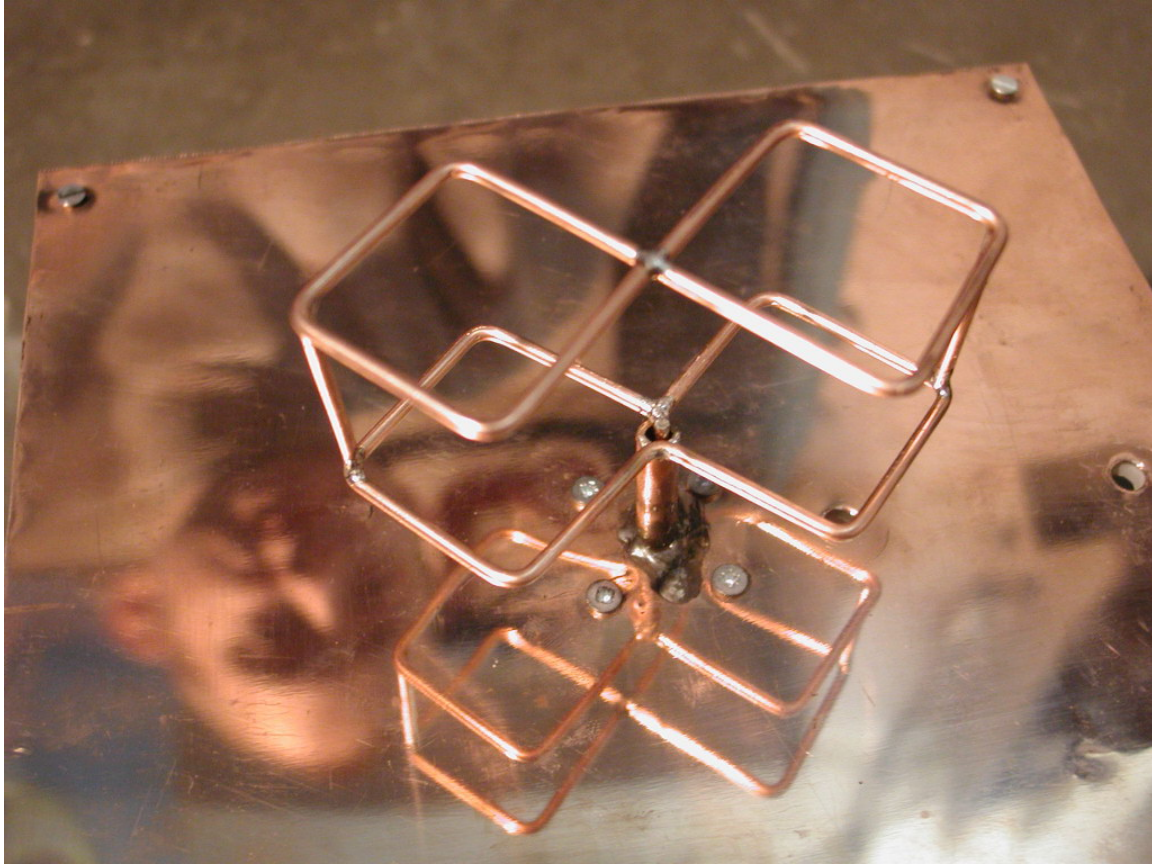


Fig. 21. Feeding of 2 el. bi-quad feed antenna

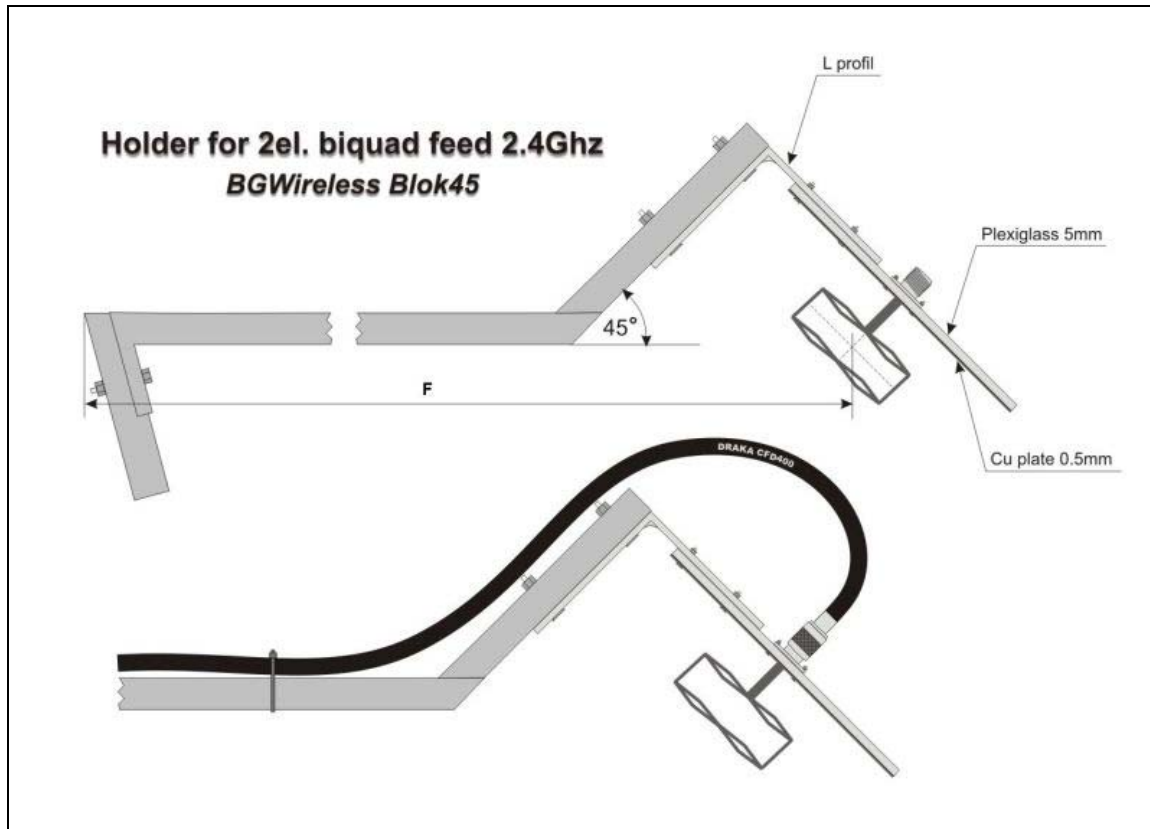


Fig. 22. Example of holder for 2 el. bi-quad feed antenna

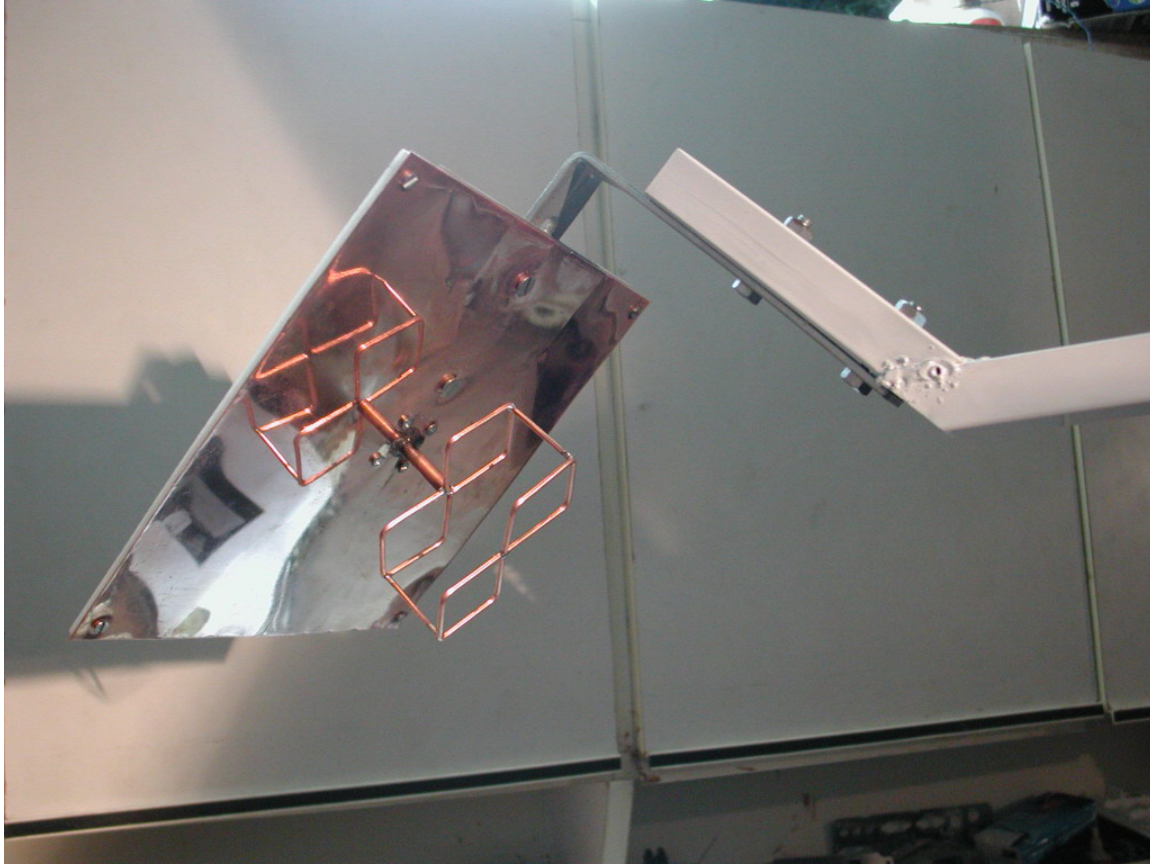


Fig. 23. Two-elements bi-quad feed antenna on its carrier



Fig. 24. Offset dish with 2 el. bi-quad feed antenna

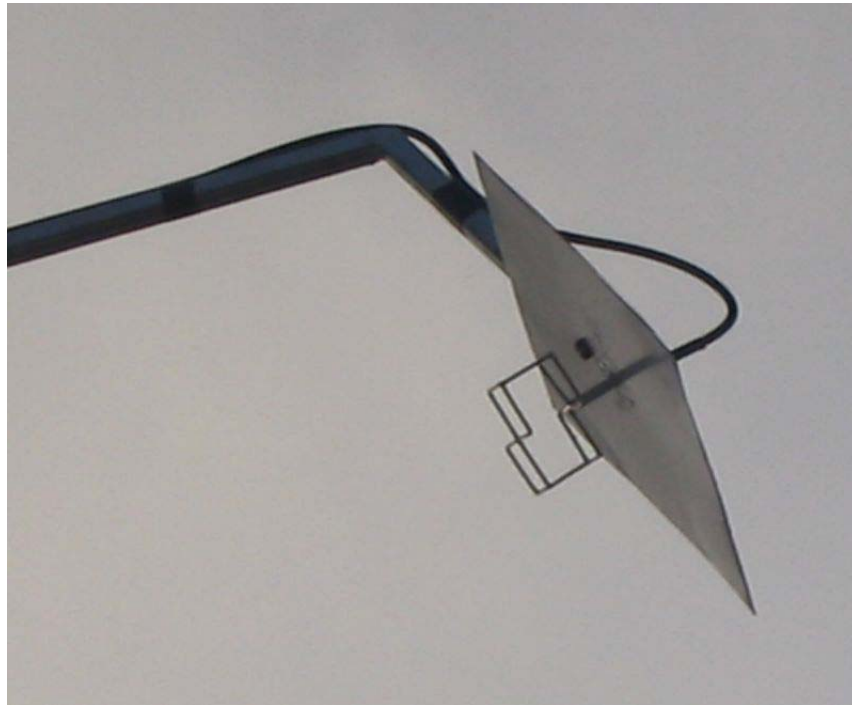


Fig. 25. Close-up view of 2 el. bi-quad feed antenna mounted on carrier

Conclusion

In this article we showed and, by precise computer simulations [6] and practical measurements, confirmed the possibility of using a two-element bi-quad for efficient illumination SAT TV offset parabolic mirror. The very pure and symmetrical diagram of two-element bi-quad, with equal width of the main beam in both planes, proved to be a very efficient feed for offset parabolic antennas whose F/D is 0.7-0.9. -30-

Literature

1. Optimal bi-quad at: <http://www.cebik.com/vhf/planar3.html>
2. 3D corner reflector feed antenna for 5.8 GHz (*antenneX*, issue number 126)
3. The W1GHZ Online Microwave Antenna Book
4. A.W. Love, *Reflector Antennas*, IEEE Press, 1978.
5. John Kraus, *Antennas*, McGraw Hill, 1956.
6. 4NEC2, NEC based antenna modeler and optimizer by Arie Voors

BRIEF BIOGRAPHY OF THE AUTHOR



Dragoslav Dobričić, YU1AW, is a retired electronic engineer and worked for 40 years in Radio Television Belgrade on installing, maintaining and servicing radio and television transmitters, microwave links, TV and FM repeaters and antennas. At the end of his career, he mostly worked on various projects for power amplifiers, RF filters and multiplexers, communications systems and VHF and UHF antennas.

For over 40 years, Dragan has published articles with different original constructions of power amplifiers, low noise preamplifiers, antennas for HF, VHF, UHF and SHF bands. He has been a licensed Ham radio since 1964. Married and has two grown up children, a son and a daughter.

antenneX Online Issue No. 128 — December 2007

Send mail to webmaster@antennex.com with questions or comments.

Copyright © 1988-2007 All rights reserved - *antenneX*©